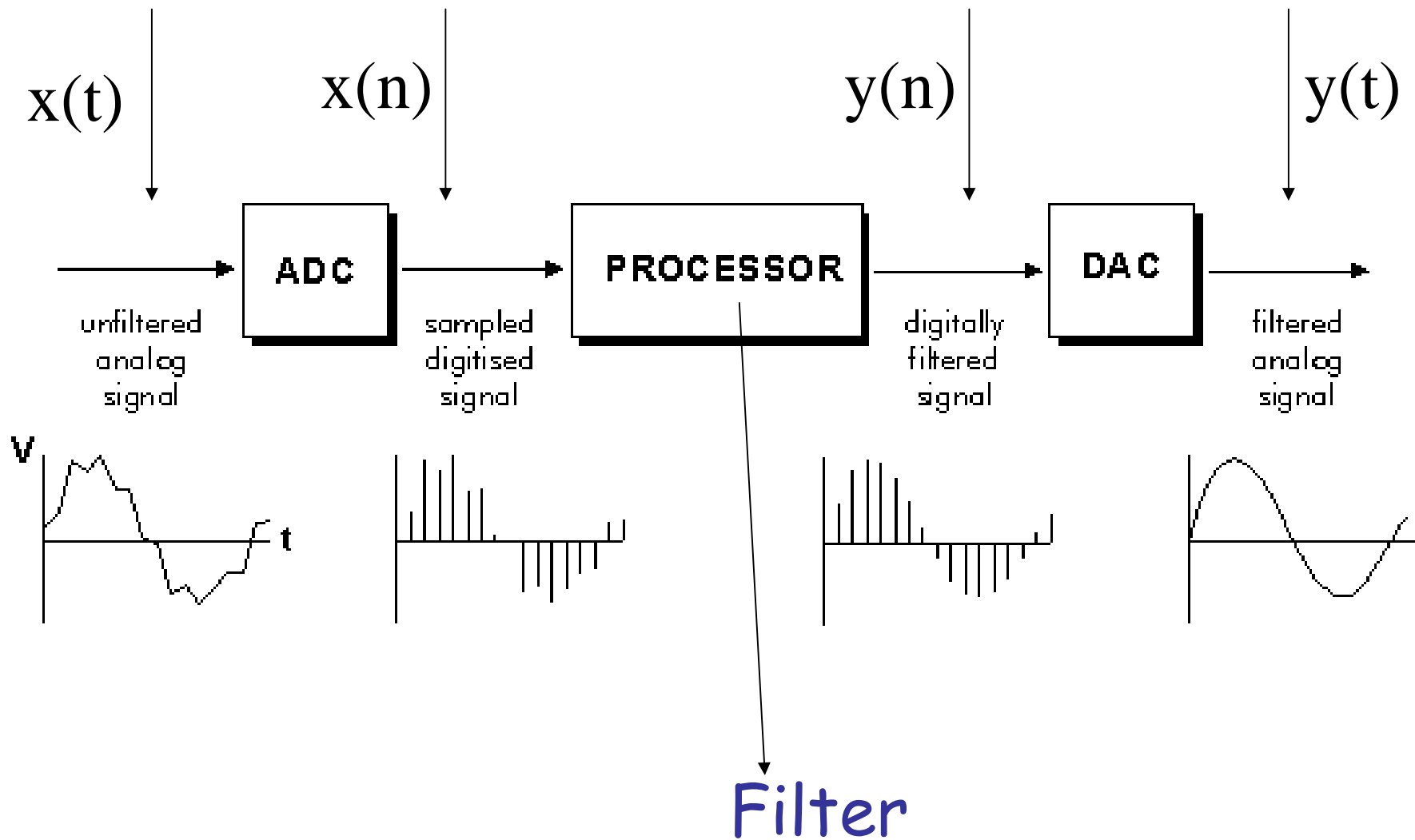


Finite Response Filters or FIR Filters

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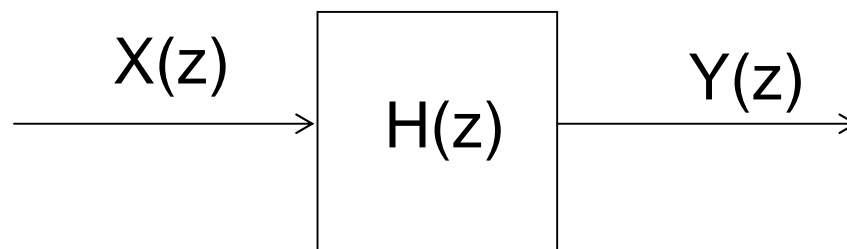
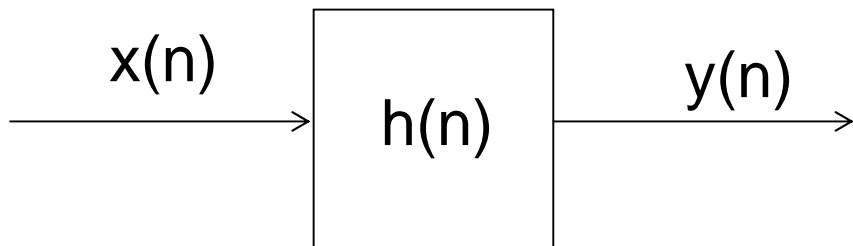
A filter is a frequency selective device

Passes certain band of frequencies and
Blocks frequencies out of this band.

A Digital Filter is a mathematical algorithm
that operates on a discrete time signal ($x(n)$, input),
to produce a discrete time output signal ($y(n)$, output),
to achieve the filtering objective.

The digital filter is characterized by its
Impulse Response ($h(n)$)

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Block Diagram Representation

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Digital Systems are characterised by Linear Constant Coefficient Difference equation(LCCDE)

$$y(n) = \sum_{k=0}^M b_k x(n-k) - \sum_{k=1}^N a_k y(n-k)$$

$$y(n) = b_0 x(n) + b_1 x(n-1) + \dots + b_M x(n-M) \\ - [a_1 y(n-1) + a_2 y(n-2) + \dots + a_N y(n-N)]$$

Output depends on present and past inputs and past outputs

-- Mrs. Aarti Bāng, Infinite Impulse Response (IIR) Systems

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Output depends on present and past inputs only
----- Finite Impulse Response (FIR) Systems

$$y(n) = \sum_{k=0}^M b_k x(n-k)$$

$$y(n) = b_0 x(n) + b_1 x(n-1) + \dots + b_M x(n-M)$$

$$y(n) = h_0 x(n) + h_1 x(n-1) + \dots + h_M x(n-M)$$

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Alternative Representation is (in Z - Domain)

$$H(z) = \frac{\sum_{k=0}^M b_k z^{-k}}{1 + \sum_{k=1}^N a_k z^{-k}}$$

IIR System

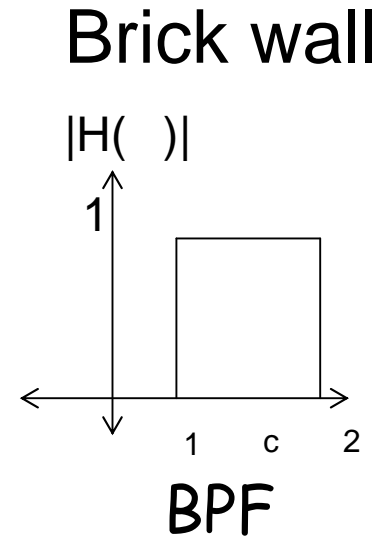
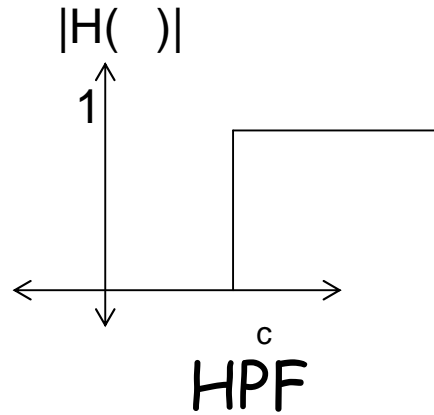
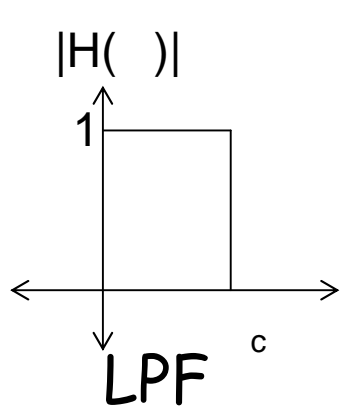
$$H(z) = \sum_{k=0}^M b_k z^{-k}$$

FIR System

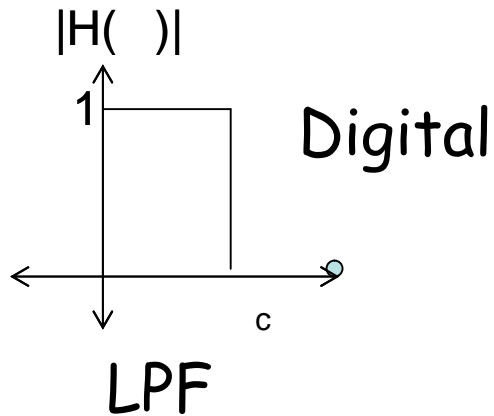
$$H(z) = \sum_{k=0}^M h_k z^{-k}$$

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Filter Characteristics



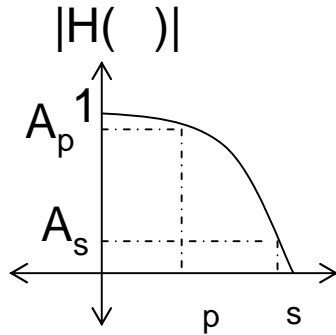
Analog



⋮

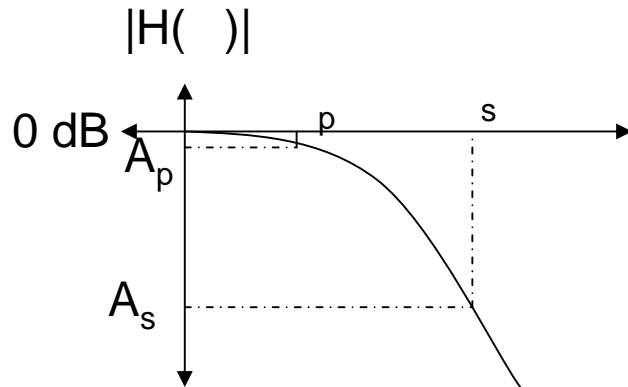
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Practical Characteristics



A_p is minimum pass band gain
 A_s is maximum stop band gain
 ω_p is the pass band edge frequency
 ω_s is the stop band edge frequency

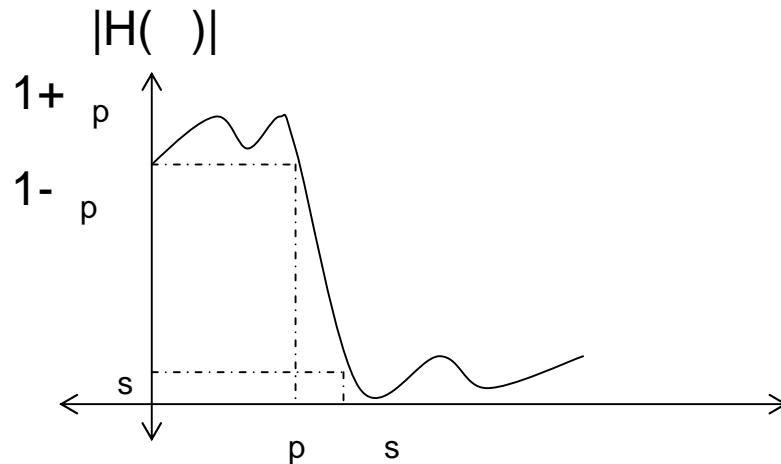
Gain Characteristics



A_p in dB is maximum pass band attenuation
 A_s in dB is minimum stop band attenuation
 ω_p is the pass band edge frequency
 ω_s is the stop band edge frequency

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Attenuation Characteristics



$\delta_p \rightarrow$ pass band ripple

$\delta_s \rightarrow$ stop band ripple

$$A_p = 1 - \delta_p$$

$$A_p = -20 \log_{10}(1 - \delta_p) \text{ db}$$

$$A_s = -20 \log_{10}(\delta_s) \text{ db}$$

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Order of Filter : (N or M)

The rate at which gain decreases from pass band to stop band, along the frequency.

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Ideal filters have

- Constant Magnitude characteristics
- Linear Phase characteristics

within the pass band

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A filter has linear phase response if

$$y(n) = cx(n-n_0)$$

i.e. output is simply delayed and amplitude scaled version of input.

Linear phase characteristics can be written as

$$\Theta(\omega) = -\omega n_0 \quad (\text{negative sign is for phase lag})$$

$$\frac{d\Theta(\omega)}{d\omega} = -n_0 = \tau_g(\omega) \quad \begin{array}{l} \text{Group delay or} \\ \text{Envelope delay} \\ \text{that is constant} \end{array}$$

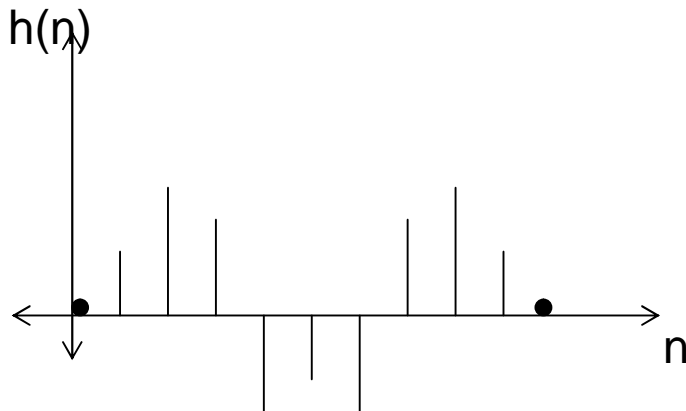
i.e. all frequency components of the input signal undergo same (constant) time delay.

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FIR filters have linear phase response if their impulse response is symmetric or antisymmetric

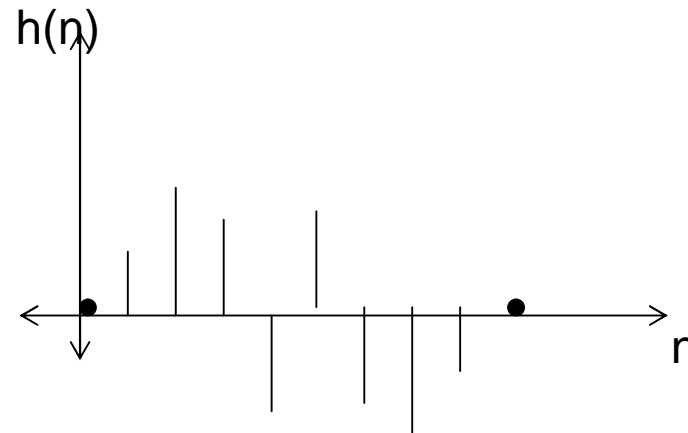
$$h(n) = h(M-1-n)$$

Here $M=11$



$$h(n) = -h(M-1-n)$$

Here $M=10$



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Characteristics of FIR filters :

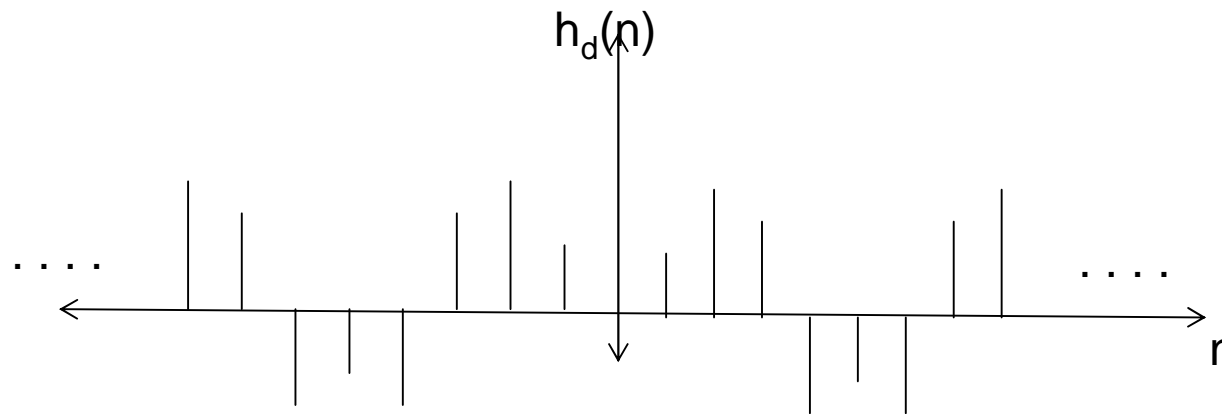
Have **linear phase response**

Are inherently **stable**

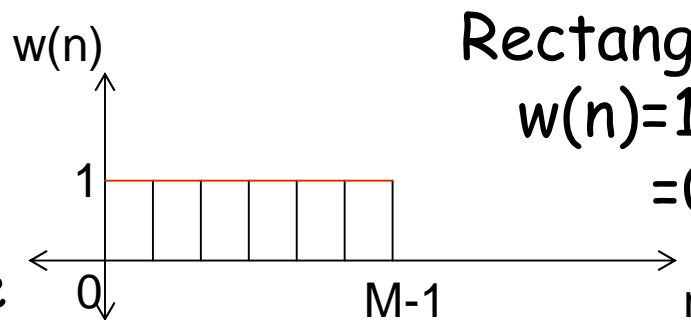
Are **all zero** systems

Need **higher order** for similar magnitude

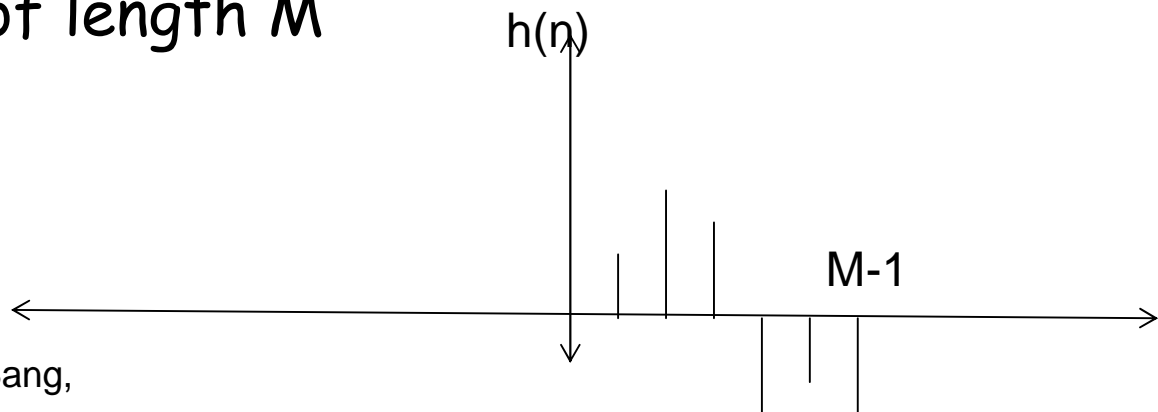
Design of FIR filters means,
design of unit sample response $h(n)$, means
design of M coefficients $h(n)$, $n=0,1,\dots,M-1$ from a
desired frequency response $H_d(\omega)$



This is equivalent of multiplying $h_d(n)$ by a window sequence $w(n)$ of length M



Rectangular window
 $w(n)=1 \quad n=0,1,\dots,M-1$
 $=0 \quad \text{otherwise}$



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Methods for designing FIR filters

- Window method
- Frequency Sampling method

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Design of FIR filters using Window method

$H_d(\omega)$ → desired frequency response of digital filter

$h_d(n)$ → corresponding impulse/unit sample response

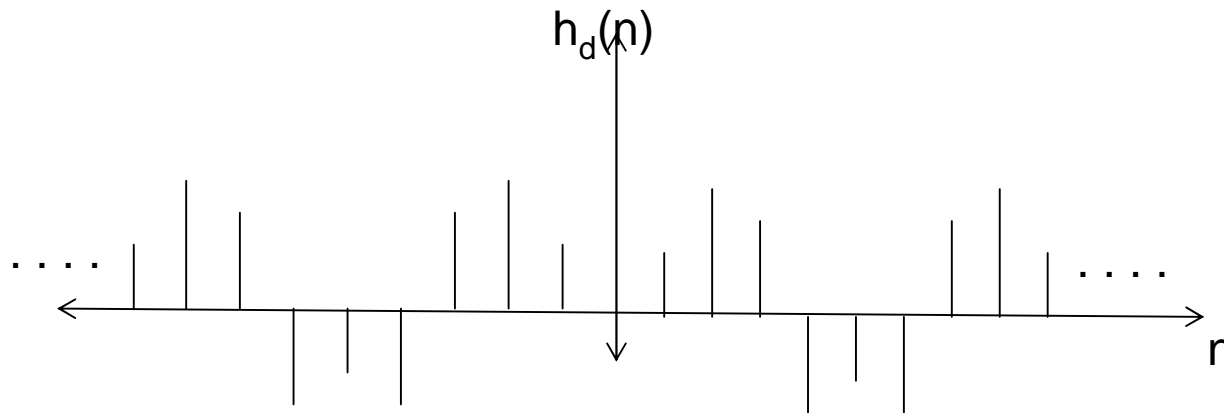
$$H_d(\omega) = \sum_{n=0}^{\infty} h_d(n) e^{-j\omega n}$$

$$h_d(n) = \frac{1}{2\pi} \int_{-\pi}^{\pi} H_d(\omega) e^{-j\omega n} d\omega$$

Discrete Time Fourier Transform pair eq.

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The unit sample response $h_d(n)$, obtained, is Infinite in duration and Non-causal
→ Non-realizable



$h_d(n)$ should be made finite and causal.
i.e. truncated to length M .

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Steps in designing FIR filter using window method

- Given $H_d(\omega)$
- Determine $h_d(n)$, using Inverse Fourier Transform
- Compute $h(n) = h_d(n) \times w(n)$ $n=0,1,\dots,M-1$

Specifications given are:

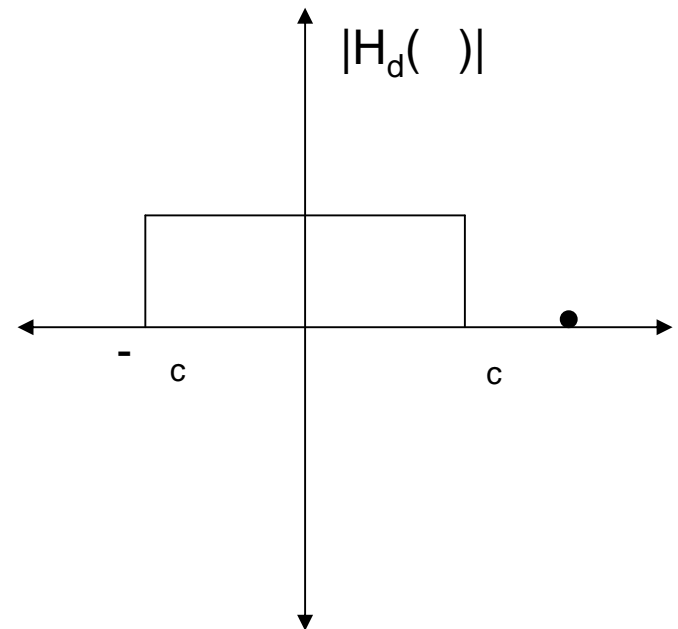
$$H_d(\omega) = 1 \quad | \omega | \leq \omega_c$$

$$= 0 \quad \omega_c < | \omega | \leq \omega_p$$

$$H_d(\omega) = e^{-j \tau \omega} \quad | \omega | \leq \omega_c$$

$$= 0 \quad \omega_c < | \omega | \leq \omega_p$$

where $\tau = (M-1)/2$



$$h_d(n) = \frac{1}{2\pi} \int_{-\pi}^{\pi} H_d(\omega) e^{j\omega n} d\omega$$

$$h_d(n) = \frac{1}{2\pi} \int_{-\omega_c}^{\omega_c} e^{-j\omega\tau} e^{j\omega n} d\omega$$

$$h_d(n) = \frac{1}{(n-\tau)\pi} [\sin\omega_c(n-\tau)]$$

for n not equal τ

$$h_d(n) = \frac{\omega_c}{\pi} \quad \text{for } n = \tau$$

What is τ ?

If filter is symmetric,
 $h_d(n) = h_d(M-1-n)$

$$\frac{\sin\omega_c(n-\tau)}{(n-\tau)\pi} = \frac{\sin\omega_c(M-1-n-\tau)}{(M-1-n-\tau)\pi}$$

$$-(n-\tau) = M-1-n-\tau$$

$$\tau = (M-1)/2$$

$$h_d(n) = \frac{\sin\omega_c\left(n - \frac{M-1}{2}\right)}{\left(n - \frac{M-1}{2}\right)\pi}$$

for n not equal τ

$$h_d(n) = \frac{\omega_c}{\pi}$$

for $n = \tau$

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Effect of Rectangular window function on desired frequency response

$$w(n) = \begin{cases} 1 & n=0,1,\dots,M-1 \\ 0 & \text{otherwise} \end{cases}$$

Impulse response of FIR filter is
 $h(n) = h_d(n) \times w(n)$

Multiplication in time domain is equivalent to Convolution in frequency domain.

$$H(\omega) = \frac{1}{2\pi} \int_{-\pi}^{\pi} H_d(\omega) W(\omega - \nu) d\nu$$

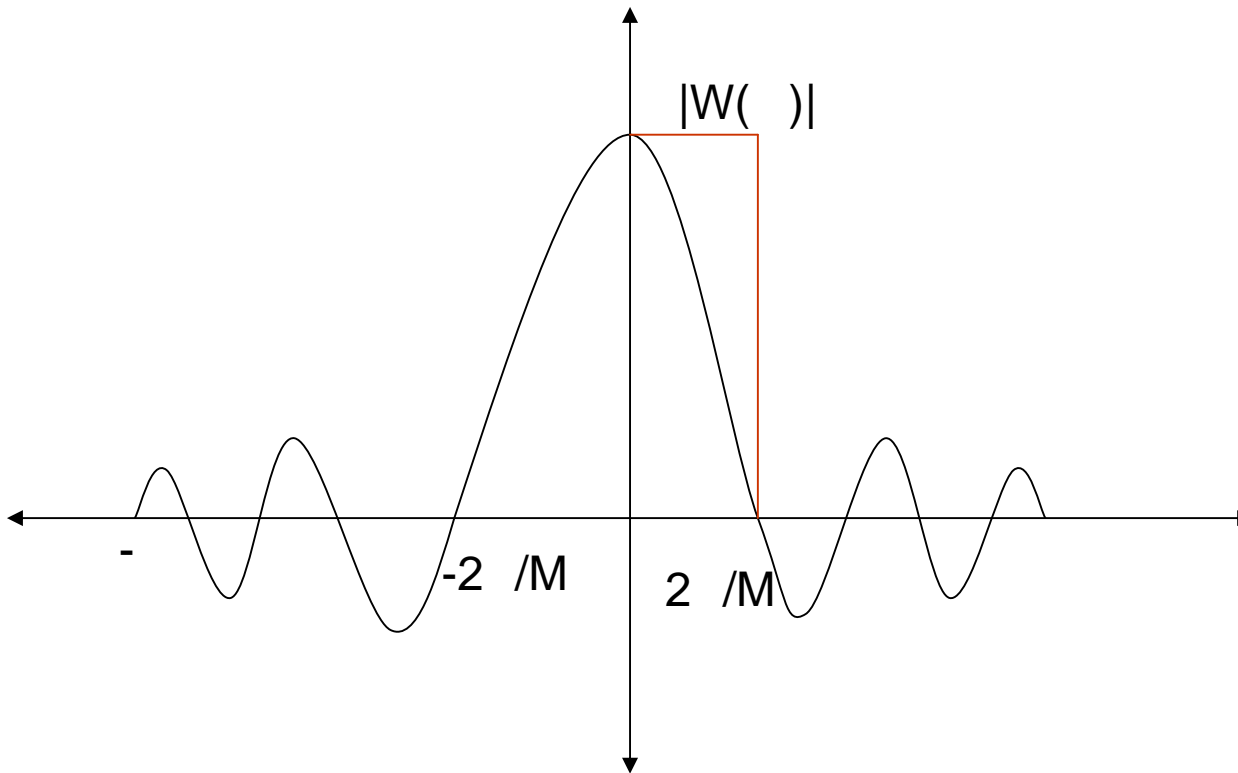
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Fourier Transform of window function is

$$W(\omega) = \sum_{n=0}^{M-1} e^{-j\omega n}$$

$$W(\omega) = \frac{1 - e^{-j\omega M}}{1 - e^{-j\omega}} = e^{-j\omega \frac{M-1}{2}} \frac{\sin \frac{\omega M}{2}}{\sin \frac{\omega}{2}}$$

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Frequency response of rectangular window

- There is main lobe, contains most of the energy, width is $4/M$
- There are a no. of side lobes that decay rapidly.
- As M increases, width of main lobe becomes narrow.
- Height of each side lobe increases as M increases
- Width of each side lobe decreases as M increases.
- Area of each side lobe remains unchanged.

- The truncation of infinite series results in undesirable oscillations in the pass band and stop band.
 - These oscillations are due to abrupt discontinuity at the edge of window.
 - These oscillations can be reduced using a tapered window.
-
- The oscillatory behaviour near the band edge of filter is called Gibbs phenomenon.

Desirable characteristics of window function :

The Fourier Transform/Frequency response of window function should have a small width main lobe containing as much as the total energy as possible.

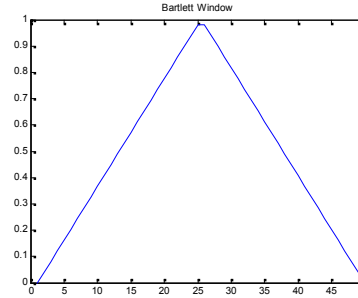
It should have side lobes that decrease in energy rapidly as w tends to ∞ .

Window Functions

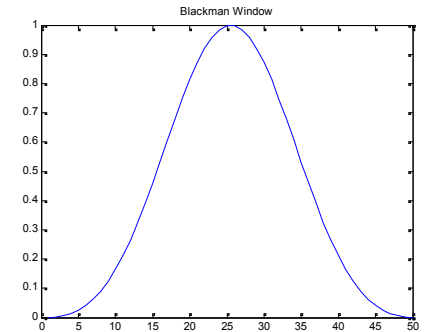
$$w(n), \quad 0 \leq n \leq M-1$$

Bartlett
(Triangular)

$$1 - \frac{2 \left| n - \frac{M-1}{2} \right|}{M-1}$$

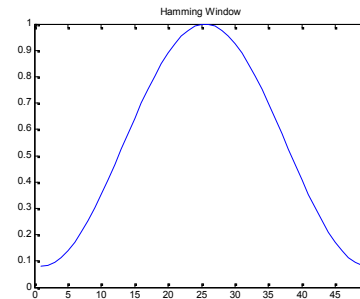


Blackman $0.42 - 0.5 \cos \frac{2\pi n}{M-1} + 0.08 \cos \frac{4\pi n}{M-1}$



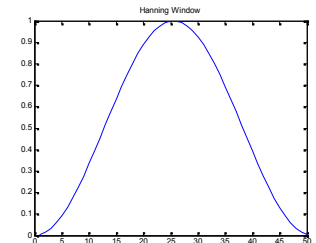
Hamming

$$0.54 - 0.46 \cos \frac{2\pi n}{M-1}$$



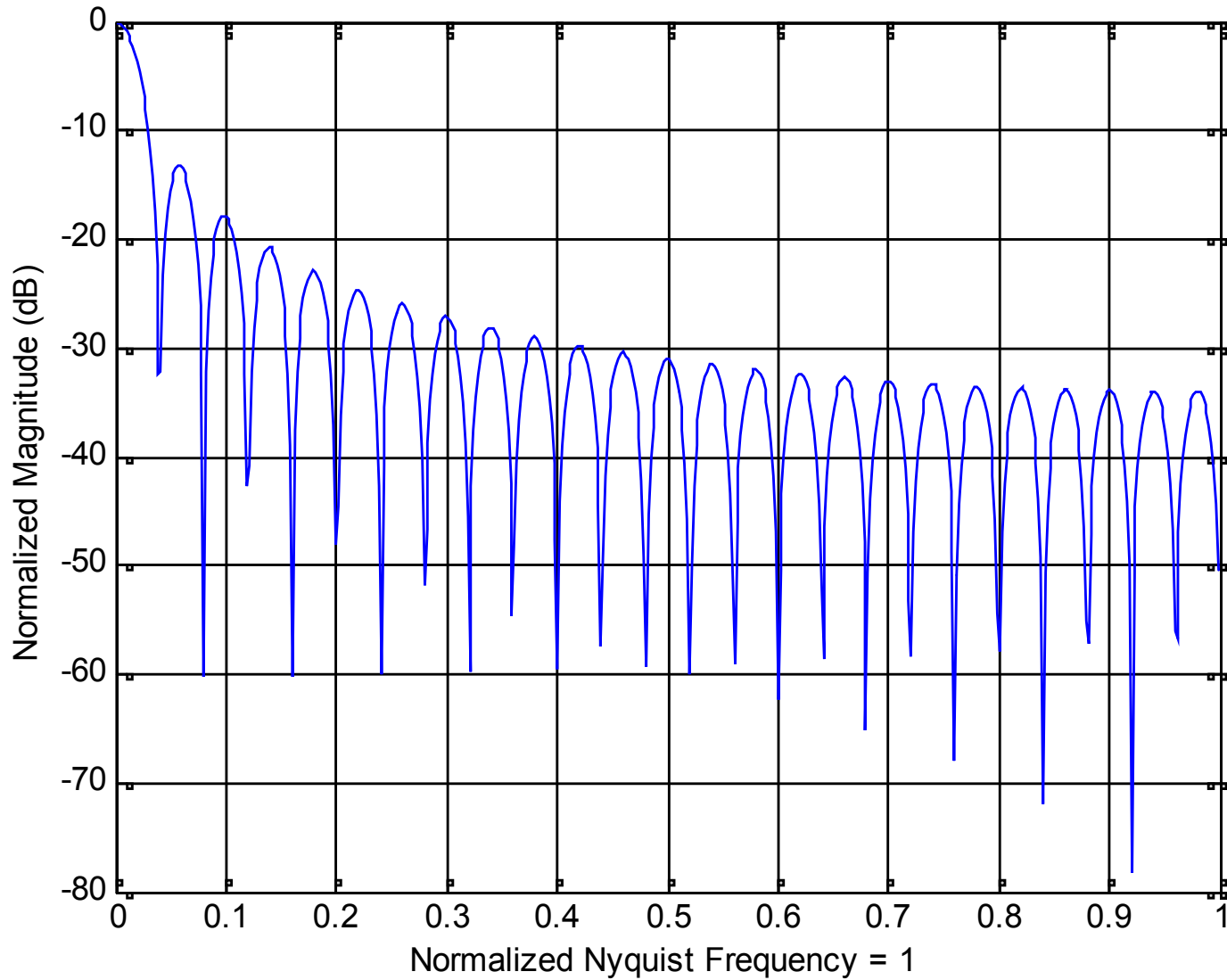
Hanning

$$\frac{1}{2} \left(1 - \cos \frac{2\pi n}{M-1} \right)$$



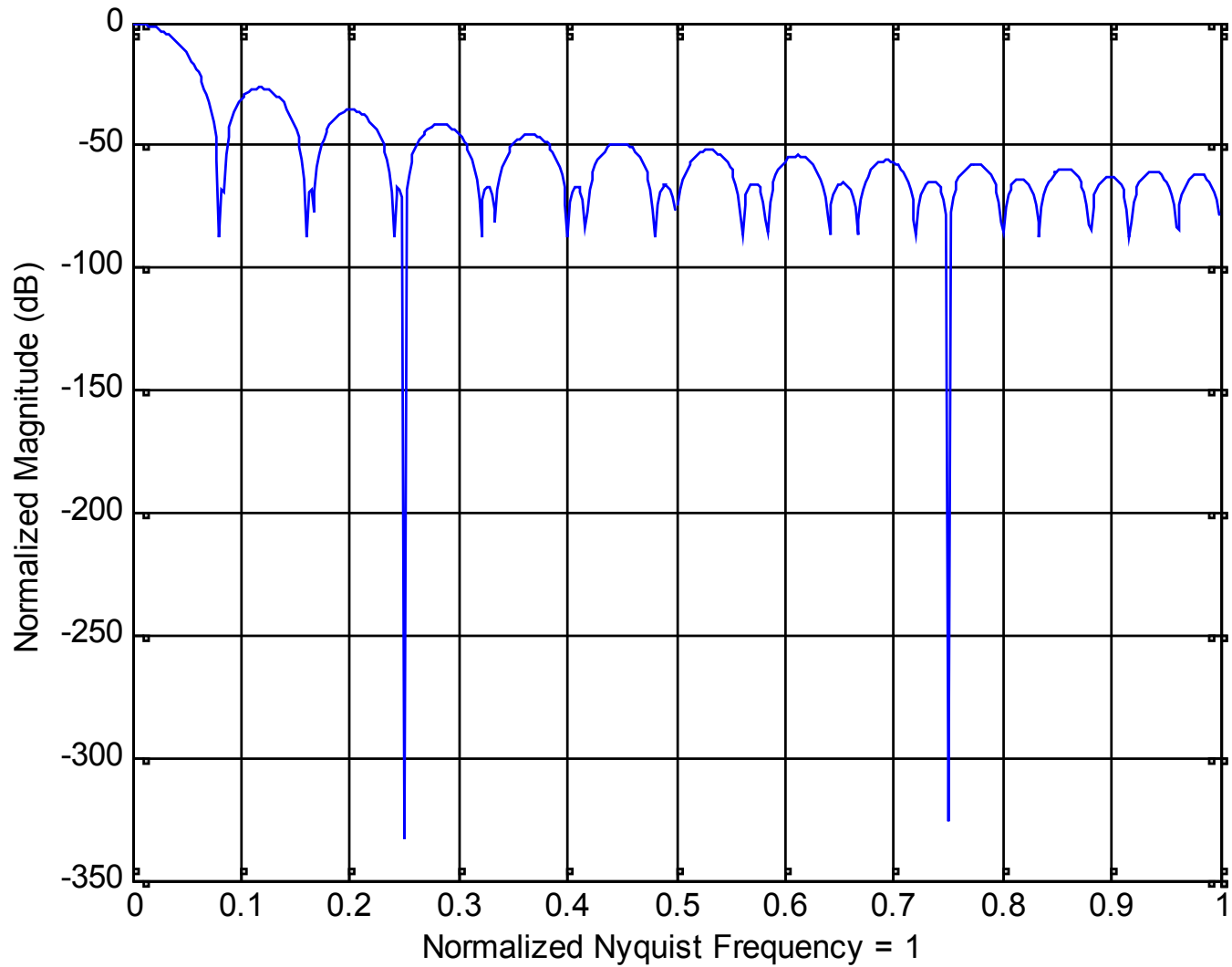
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Rectangular Window Frequency Response



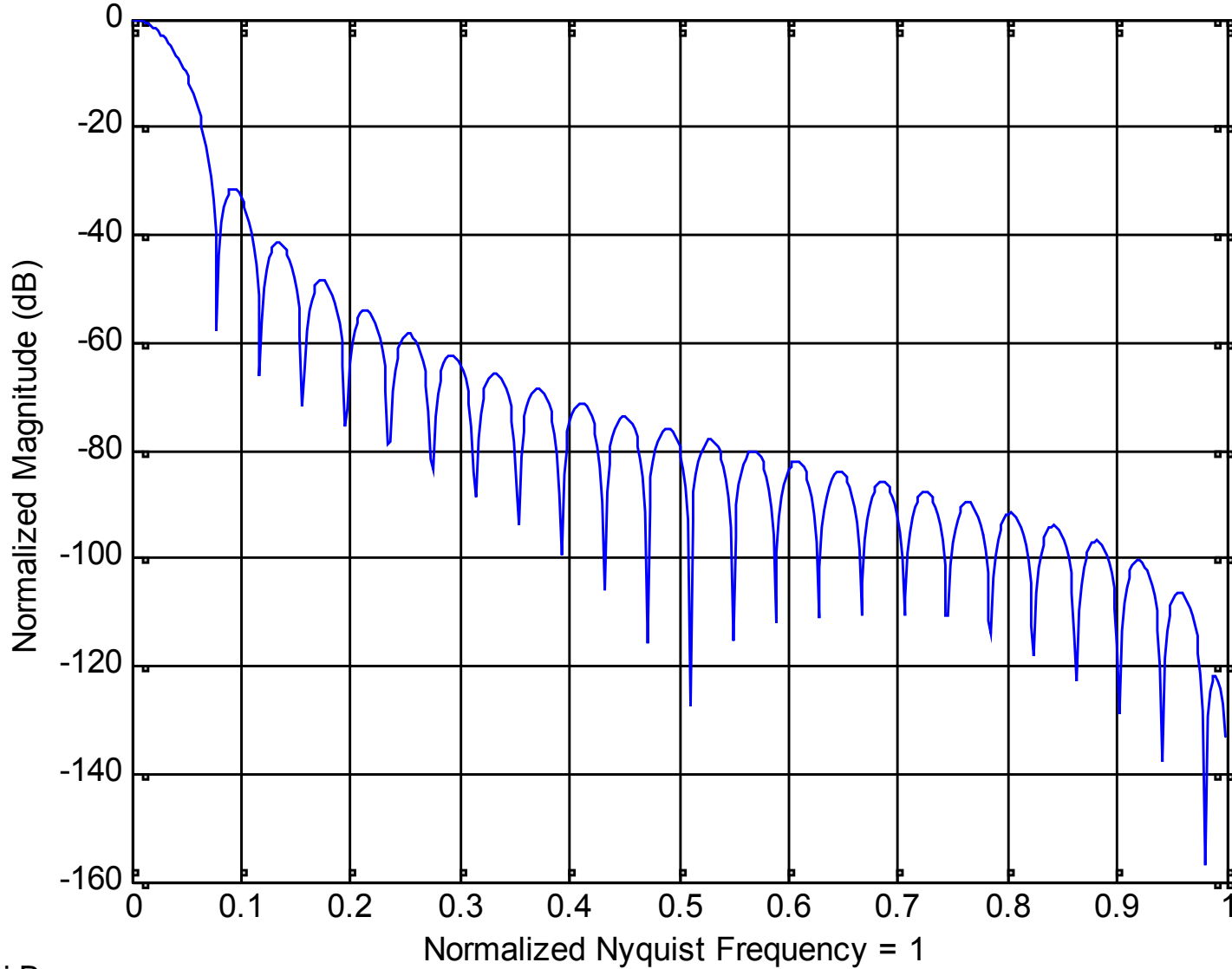
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Bartlett Window Frequency Response

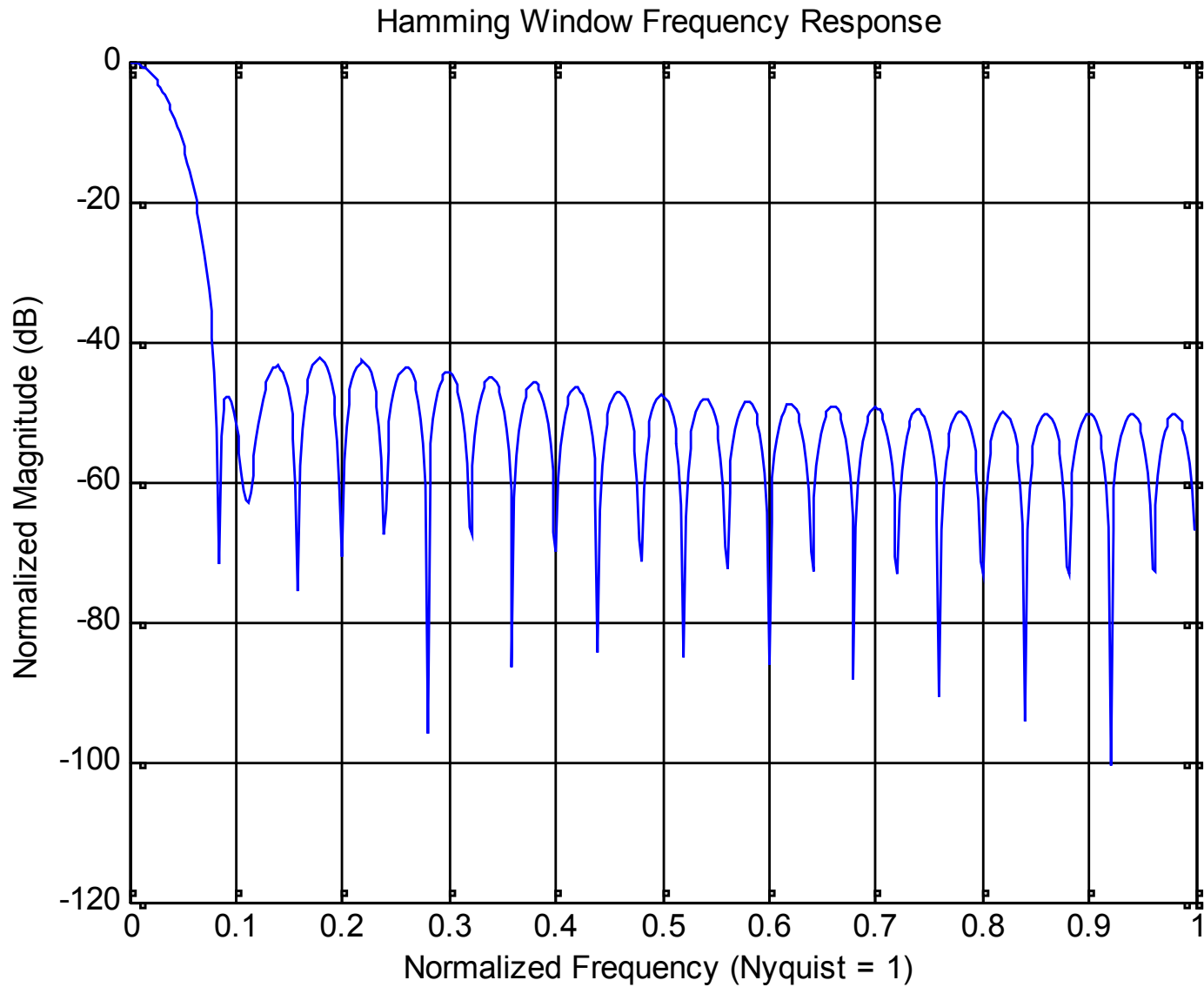


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Hanning Window Frequency Response

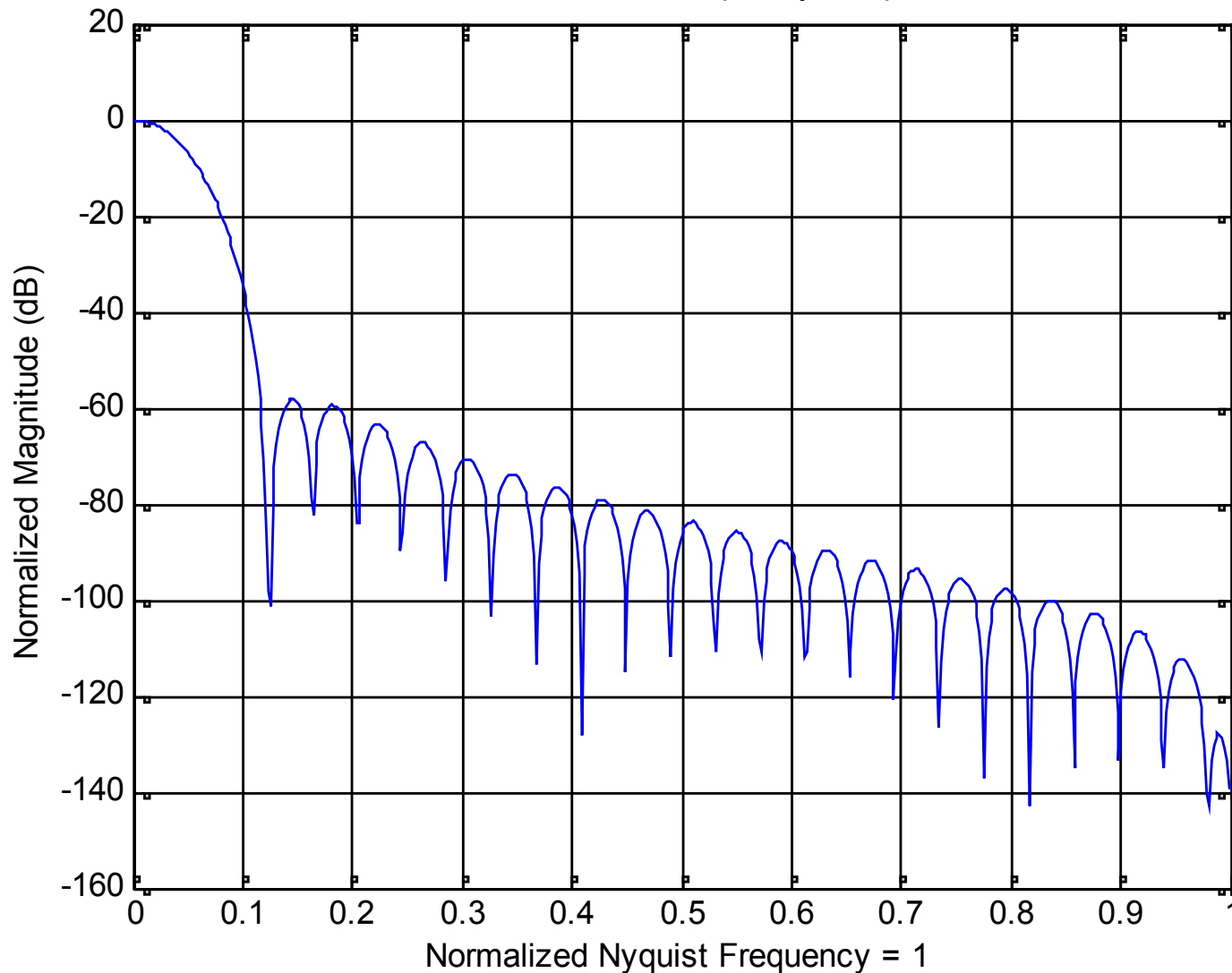


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Blackman Window Frequency Response



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Type of Window	Width of Main Lobe	Min. Stopband Attenuation (db)	Peak side Lobe (db)	Normalized Transition width Δf
Rectangular	$4/M$	-21	-13	$0.9/M$
Bartlett	$8/M$	-25	-27	
Hanning	$8/M$	-44	-32	$3.1/M$
Hamming	$8/M$	-53	-43	$3.3/M$
Blackman	$12/M$	-74	-58	$5.5/M$

Window Functions :

- Minimize the ringing effects at the band edge.
- Result in lower side lobes.
- **At the expense of increase in the width of transition band.**

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Estimation of Filter Order (M) :

Kaiser's formula:

$$M = \frac{-10 \log_{10} (\delta_p \delta_s) - 13}{14.6 \Delta f}$$

or

$$M = \frac{-10 \log_{10} (\delta_p \delta_s) - 13}{14.6 (\omega_{st} - \omega_p) P / 2\pi}$$

M is inversely proportional to transition bandwidth ($\omega_s - \omega_p$)
and not on transition band location.

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Estimation of Filter Order (M) :

- **Hermann-Rabiner-Chan's Formula:**

$$M \cong \frac{D_{\infty}(\delta_p, \delta_s) - F(\delta_p, \delta_s)[(\omega_s - \omega_p) / 2\pi]^2}{(\omega_s - \omega_p) / 2\pi}$$

where

$$D_{\infty}(\delta_p, \delta_s) = [a_1(\log_{10} \delta_p)^2 + a_2(\log_{10} \delta_p) + a_3] \log_{10} \delta_s \\ + [a_4(\log_{10} \delta_p)^2 + a_5(\log_{10} \delta_p) + a_6]$$

$$F(\delta_p, \delta_s) = b_1 + b_2[\log_{10} \delta_p - \log_{10} \delta_s]$$

with

$$a_1 = 0.005309, a_2 = 0.07114, a_3 = -0.4761$$

$$a_4 = 0.00266, a_5 = 0.5941, a_6 = 0.4278$$

$$b_1 = 11.01217, b_2 = 0.51244$$

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FIR Digital Filter Order Estimation

- Formula valid for $\delta_p \geq \delta_s$
- For $\delta_p < \delta_s$, formula to be used is obtained by interchanging δ_p and δ_s
- Both formulae provide only an estimate of the required filter order N
- If specifications are not met, increase filter order until they are met

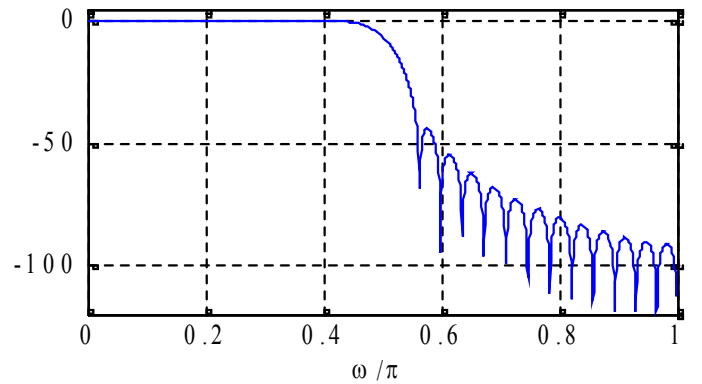
Steps in designing FIR filter

- Specify the desired frequency response $H_d(\omega)$
- Select a window function that satisfies the attenuation specification
- Determine the no. of filter coefficients (M) using the relationship between M & Δf
- Obtain impulse response $\underline{h_d(n)}$ by evaluating inverse fourier transform
- Obtain M values of chosen window function, $\underline{w(n)}$
- Obtain actual FIR coefficients, $\underline{h(n)}$, using the relation
$$h(n) = h_d(n) \times w(n)$$

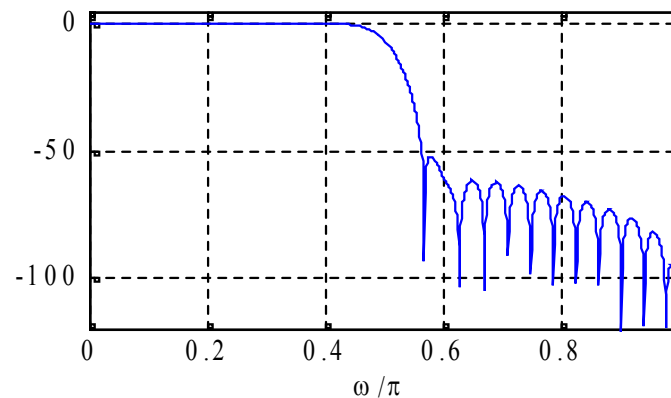
Example

- Lowpass filter of length 51 and $\omega_c = \pi / 2$

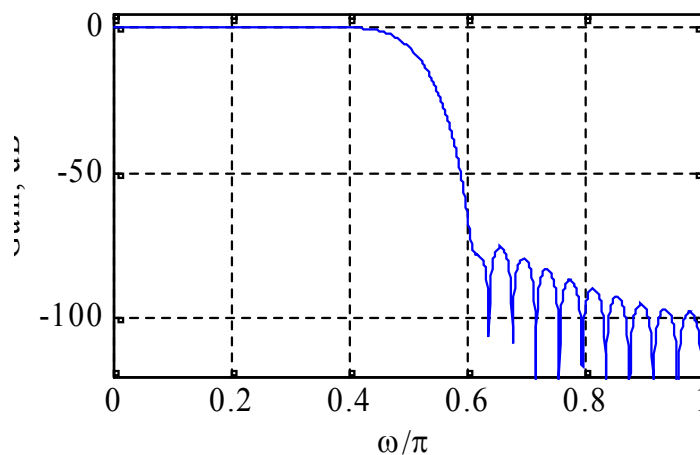
Lowpass Filter Designed Using Hann window



Lowpass Filter Designed Using Hamming window



Lowpass Filter Designed Using Blackman window



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Kaiser Window

$$w(n) = \frac{I_0 \left[\beta \sqrt{1 - \left(\frac{2n}{M-1} \right)^2} \right]}{I_0[\beta]}$$

$$-(M-1)/2 \leq n \leq (M-1)/2$$

elsewhere

$$= 0$$

- where $I_0(x)$ is the zero-order modified Bessel function of the first kind.
- & M controls the way window function tapers at the edges.
- & M controls the ripple, the stopband attenuation & transition width
- & M is determined by stopband attenuation requirements.

$$= \min(p, s) \quad A = -20 \log_{10}$$

$$= 0$$

$$A \leq 21 \text{ dB}$$

$$= 0.5842(A - 21)0.4 + 0.07886(A - 21) \quad 21 \text{ dB} < A < 50 \text{ dB}$$

$$= 0.1102(A - 8.7)$$

$$A \geq 50 \text{ dB}$$

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Length of filter (Kaiser window) is given by

$$M \geq \frac{\delta_s - 7.95}{14.36\Delta f}$$

where Δf is the normalized transition width

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Example: Kaiser Window Design of a Low pass Filter

- Specifications $\omega_p = 0.4\pi, \omega_s = 0.6\pi, \delta_1 = 0.01, \delta_2 = 0.001$
- Window design methods assume $\delta_1 = \delta_2 = 0.001$
- Determine cut-off frequency
 - Due to the symmetry we can choose it to be $\omega_c = 0.5\pi$

- Compute

$$\Delta\omega = \omega_s - \omega_p = 0.2\pi$$

$$A = -20 \log_{10} \delta = 60$$

- And Kaiser window parameters

$$\beta = 5.653$$

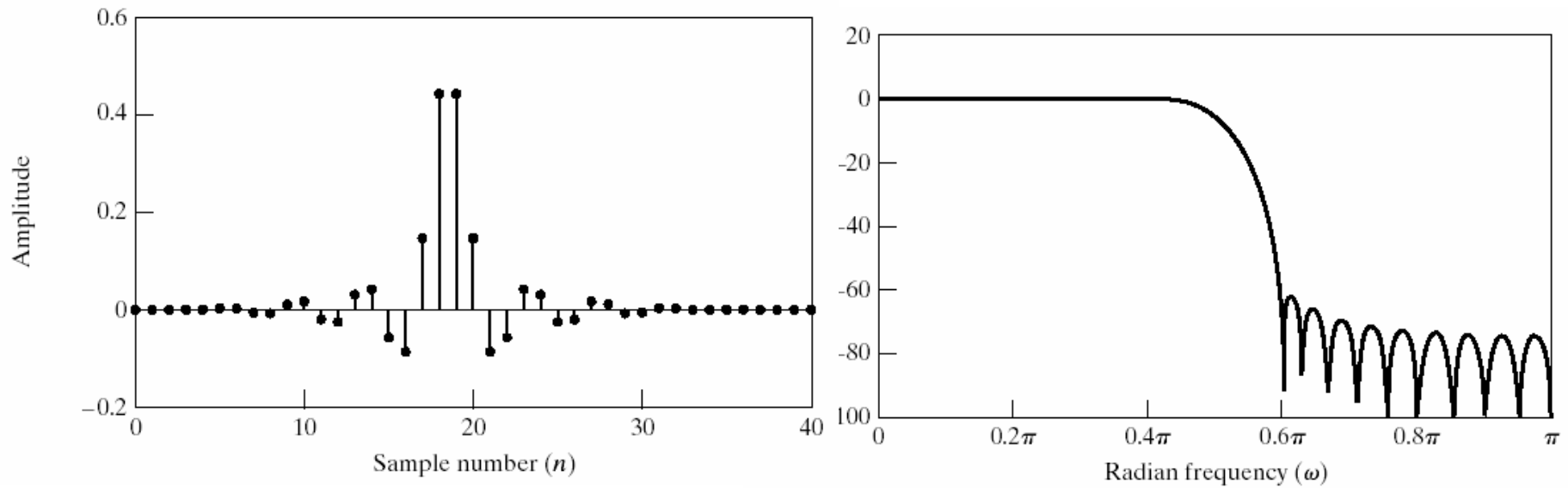
$$M = 37$$

- Then the impulse response is given as

$$h[n] = \begin{cases} \frac{\sin[0.5\pi(n - 18.5)]}{\pi(n - 18.5)} \frac{I_0 \left[5.653 \sqrt{1 - \left(\frac{n - 18.5}{18.5} \right)^2} \right]}{I_0(5.653)} & 0 \leq n \leq M \\ 0 & \text{else} \end{cases}$$

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Example Cont'd



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